

Sustainable enhancement of coal seam gas production in Queensland

Development of new technologies for upgrading the return on what is currently uneconomic or marginally economic

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Presentation Agenda

- Some commercial aspects of the CSG industry
- Production challenges in Surat and Bowen Basins
- The effect of stress and material heterogeneity
- Current practice in the prediction of hydraulic fractures and permeability increase in CSG wells
- Development of advanced predictive capabilities:
 - Near-wellbore stress and fracture initiation
 - Complex, three-dimensional fracture propagation
 - Propagation of proppant into natural fractures
- Future research, including the incorporation of production forecasting and uncertainty analysis





Centre for Natural Gas





CSG and LNG in Eastern Australia

- East-coast, on-shore gas market in Australia well positioned to produce CSG-LNG for at least the next thirty years
- Approximately \$9 billion in LNG exports in 2016-17, when only at 75% capacity
- Environmental, economic and political drivers to increase production from assets
 - Less CO2 intensive source of energy
 - Demand for electricity/manufacturing
 - State and federal policies to promote increased production and exploration
- However, significant volumes of gas remain classified as 3C resources
- Production challenges contributing to the write-down of some reserves



https://www.data.qld.gov.au/dataset/petroleum-gas-production-and-reserve-statistics



Production Challenges in the Surat and Bowen Basins

- Production outcomes from hydraulic fracture stimulations not universally repeatable
- Bowen Basin coals thick and continuous, can be drilled and produced from horizontal wells without hydraulic fracturing
- Surat Basin coals occur in multiple thin seams (0.1~0.5m thickness) with clastic interburden
- Complex rock mechanical properties
 - Low Young's modulus, high Poisson's ratio
 - Varying connectivity of fractures and cleats
- Stress regime varies between reverse faulting, strike-slip, and normal faulting with depth
 - Can manifest as stress barrier to fractures
 - Evidence of non-planar fracture growth

Prov.	Age			Palynology Zones	Stratigraphy		
	90-		e				
			La	PK7			
	100-	etaceous	Late Early	PK6			
	110-			PK5	Rolling Downs Group	Griman Creek Formation	
				PK4		Surat Siltstone	
	-	C		PK3		Wallumbilla Formation	
	130-			PK2	8lythesdale Group	Bungil Formation	
				PK1		Mooga Sandstone	
i.	140-					Orallo Formation	
t Ba:	150-			PJ6	Injune Creek I Group	Westbourne Formation	
La				P 15		Springbok Sandstone	
Su	160-	ırassic	Middle	PJ4		Walloon Coal Measures	
	170-				Bundamba Group	Hutton cct	
	180-	٦ ا		PJ3		Hutton sst	
	190-		Early			Evergreen Fm	
	170			PJ2		boxvale SSE Member	
	200-			PJ1		Precipice Sst	

The geology of the Surat Basin, Australia (reproduced from Pandey and Flottmann, SPE-173378-MS)



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Calculated log properties from a well in the Surat Basin, Australia (reproduced from Pandey and Flottmann, SPE-173378-MS)



Production Challenges in the Surat and Bowen Basins



The combination of contrasting stress regime and mechanical properties manifesting as stress barriers to fractures (adapted from Tavener, Flottmann and Brooke-Barnett, 2017)



Predicting Fracture Growth during Well Completions

- The use of 2D models in 1D stress state driven by their robustness and expediency
 - Stability facilitates wide parameter studies
 - Short run times helpful in history matching
- The 1D stress model constrains planar-3D and pseudo-3D simulators when the stress regime deviates from normal (S_v > S_H > S_h)
- Non-planar fractures observed in minebacks
- Field diagnostics (e.g. microseismic, tiltmeters) has highlighted horizontal fracture growth
- A comparison of 2D simulators by Pandey and Flottmann (SPE-173378-MS) highlighted
 - Overestimation of simulated fracture height
 - Absence of observed horizontal fractures
 - Difficulty pressure-matching water treatments



Successful pressure match for a well in the Surat Basin, Australia (reproduced from Pandey and Flottmann, SPE-173378-MS)



Predicting Fracture Growth during Well Completions



Discrepancy between simulated and observed fracture geometry for a single well stage in the Surat Basin (adapted from Pandey and Flottmann, SPE-173378-MS)



Resources to Reserves: Sustaining and Increasing Supply





Research Questions

What is the near-wellbore stress state in coals, and how does it influence fracture initiation?

How do hydraulic fractures propagate in coal and clastic rocks and interact with natural fractures?



What is the injectivity of standard and novel proppant particles in CSG reservoirs?

What is the long term retained permeability of induced and natural fractures, and the stimulated reservoir volume?

What is the influence of greater understanding on production predictions, along with the associated uncertainty?

Dr Christopher Leonardi Prof Raymond Johnson Jr Dr Lukasz Laniewski Dr Ruizhi Zhong Dr Travis Mitchell Mr Bryce Hill (PhD Student) Mr Majid Fetrati (PhD Student)



The Influence of Near-Wellbore Stress on Fracture Initiation



Prediction of near-wellbore damage following drilling.

Coalescence of fractures around stage perforations.



3D FEM-DEM Modelling of a Synthetic CSG Well Stage

- Systematically vary the stress regime
 - NF = normal, SS = strike-slip, RF = reverse
- Sensitivity analysis on Young's Modulus
- Sensitivity analysis on pumping rate
- Influence of perforation orientation to stress

Madal Nama	Kh	Кн	θ	Ε	Ι
	(-)	(-)	(deg)	(GPa;MMpsi)	(bbl/min;m ³ /s)
NF1	0.6	0.8	0	6.4; 0.928	35; 0.093
SS1	0.8	1.2	0	6.4; 0.928	35; 0.093
SS1B	0.8	1.2	45	6.4; 0.928	35; 0.093
RF1	1.2	1.4	0	6.4; 0.928	35; 0.093
NF2	0.6	0.8	0	6.4; 0.928	15; 0.040
SS2	0.8	1.2	0	6.4; 0.928	15; 0.040
SS2B	0.8	1.2	45	6.4; 0.928	15; 0.040
RF2	1.2	1.4	0	6.4; 0.928	15; 0.040
NF3	0.6	0.8	0	3.2; 0.464	35; 0.093
SS3	0.8	1.2	0	3.2; 0.464	35; 0.093
SS3B	0.8	1.2	45	3.2; 0.464	35; 0.093
RF3	1.2	1.4	0	3.2; 0.464	35; 0.093



Contour plot of the vertical stress distribution in the model domain, including (inset) the orientation of the starter fracture with the y- (i.e. S_H) and z- (i.e. S_y) directions

Summary of the modelling campaign performed in this study (θ =45° indicates misalignment of S_H and starter fracture)



Normal Faulting: S'_v=10MPa; S'_H=8MPa; S'_h=6MPa; $P_p=7MPa$



Strike-Slip: S'_H=12MPa; S'_v=10MPa; S'_h=8MPa; P_p=7MPa

Transient Propagation: Normal Faulting and Strike-Slip

Strike Slip (Θ =45): S'_H=12MPa; S'_v=10MPa; S'_h=8MPa; P_p=7MPa

Reverse Faulting: S'_H=14MPa; S'_h=12MPa; S'_v=10MPa; P_p=7MPa

Injectivity and Straining of Proppant in Fractures

Closure of Propped Fractures under Closure Stress

Concluding Remarks

- Advanced computational modelling can provide new insight on the mechanics of CSG well stimulation
- The continuation of this work will incorporate productivity predictions based on enhanced stimulation
- Uncertainty must be quantified, and this is an area of ongoing research
- Repeatable, reliable and cost effective stimulation strategies will convert resources to reserves
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